

# Modelling sound-matter interaction at different scales

Rafael Delgado-Buscalioni

Universidad Autónoma de Madrid

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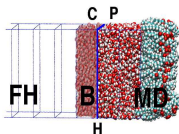
- Particle hydrodynamics
  - Florencio Balboa (Univ. Autonoma Madrid)
  - Ignacio Pagonabarraga (Univ. Barcelona) (new)
  - Anne Dejoan (CIEMAT)
- Open fluctuating hydrodynamics
  - Anne Dejoan (CIEMAT)
- Hybrid molecular-continuum hydrodynamics
  - Gianni De Fabritiis (U. Pompeu Fabra, Barcelona)
  - Jason Reese (U. StrathClyde, Glasgow) (new)
- Adaptive resolution in HybridMD
  - Matej Praprotnik (National Inst. Chem. Ljubljana)
  - Kurt Kremer (Max-Planck, Mainz)
- Coarse-grained dynamics
  - Pep Español (UNED)
  - Eric vanden-Eijnden (Courant Institute, NY)

# Multiscale approaches for complex liquids

## Domain decomposition

type A

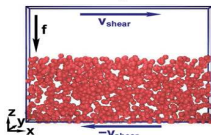
Molecular detail,  
interfases, surfaces,  
macromolecule - fluid interaction



shear flows ✓  
sound, heat ✓  
large molecules ✓  
multispecies ✗  
electrostatics ✗

## Eulerian-Lagrangian Solute-solvent hydrodynamic coupling

Suspensions  
of colloids or polymers,  
small particles in flow

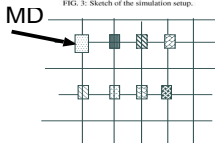


Point particle approximation:  
Stokes drag (point particle),  
Faxen terms (finite size effects)  
Basset memory effects...  
Force Coupling  
particles of finite size  
Direct simulation  
Immersed boundaries

## Patch dynamics HMM Velocity-Stress coupling

type B

Non-Newtonian fluids  
Unknown constitutive relation  
polymer melts...

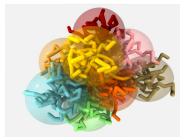


MD nodes used to  
evaluate the local stress  
for the Continuum solver.  
Continuum solver provides  
the local velocity gradient  
imposed at each MD node.

how to "lift MD" ✗

## Coarse-grained dynamics

How to reduce the  
degrees of freedom  
and keep the  
underlying dynamics



diffusion ✓  
viscosity ✓  
anisotropy ✗  
(nematics...)

## Outline of the talk

- DIRECT FORCING: **Sound-particle interactions at microns**

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  - Combining with Adaptive Resolution: the *mesoscopic buffer*.

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  - OPENMD: general ensemble

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  - OPENMD: general ensemble
  - **Test cases: Sound across MD domains**

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  - OPENMD: general ensemble
  - **Test cases: Sound across MD domains**
  - **Water wave against lipid layers**

## Direct Forcing for Point particle hydrodynamics.

### Motivation

- The Stokes drag

$$\mathbf{F}_{fp} = -\xi (\mathbf{U} - \mathbf{V})$$

- Limited to low Reynolds and small velocity gradients [Maxey, Riley]
- A practical way to relax to the zero Reynolds limit  $\mathbf{u} = \mathbf{v}_p$  [Ladd, Dünweg].
- Cannot be used to solve sound-matter interaction [Mazur, Bedeaux]
- **Direct Forcing alternative:** Get fluid-particle forces from imposition of no-slip BC at the particle center.

## Direct Forcing

based on Uhlmann, J.Comp. Phys. (2005)

**Principle:** Use a volume force  $\mathbf{F}$  to impose the velocity  $v(t)$  at one “stick point” of the fluid.

Let  $g = \rho u$  the momentum density.

$$g^{n+1} = \tilde{g}^{n+1} + f^{n+1} \Delta t$$

$$\tilde{g}^{n+1} = g^n + \mathbf{NS}^n \Delta t \quad \text{explicit solver for NS}$$

$$f^{n+1} = \rho^{n+1} \frac{v^{n+1} - \tilde{u}^{n+1}}{\Delta t} \quad \text{At the stick point } f = 0 \text{ elsewhere}$$

$$\tilde{\rho}^{n+1} = \rho^{n+1}$$

It is easy to show that this scheme satisfies:  $u^{n+1} = v^{n+1}$  at the stick point.

## Direct forcing: interpolation

Particle position  $\mathbf{R}$  in continuum space

Fluid is solved at a mesh  $\{\mathbf{r}_i\} \ i \in f$

Interpolation is required:

$$\tilde{u}(\mathbf{R}) \simeq \tilde{U} = \sum_{i \in f} \delta_h(|\mathbf{r}_i - \mathbf{R}|) \tilde{u}(\mathbf{r}_i)$$

or in brief

$$\tilde{U} = \sum_i \delta_i \tilde{u}_i$$

The kernel satisfies  $\sum_i \delta_i = 1$  and is constructed with a soft function  $\delta_h(\mathbf{r}) = \phi(x/h)\phi(y/h)\phi(z/h)$

$$\phi(u) = \begin{cases} \frac{1}{3}(1 + \sqrt{1 - 3u^2}) & 0 \leq |u| \leq \frac{1}{2} \\ \frac{1}{6}(5 - 3|u| - \sqrt{-2 + 6|u| - 3u^2}) & \frac{1}{2} \leq |u| \leq \frac{3}{2} \\ 0 & \frac{3}{2} \leq |u| \end{cases}$$

## Direct forcing: fluid-particle force

Total force exchanged between fluid and one particle:

$$\mathbf{F}(\mathbf{R}) = \rho(\mathbf{R})\Delta V\alpha = h^3 \sum_i \rho_i \mathbf{a}_i$$

$\Delta V$  is a “volume-particle parameter”

The fluid-particle relative acceleration

$$\alpha = \frac{\mathbf{V} - \tilde{\mathbf{U}}}{\Delta t}$$

is shared as acceleration of local fluid nodes,

$$\mathbf{a}_i = \alpha \delta_i \frac{\Delta V}{h^3}$$



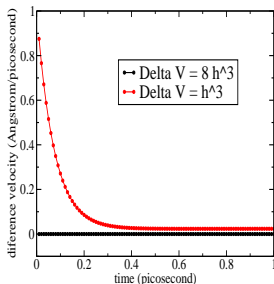
## Direct forcing: No-slip

It is easy to show that

$$\mathbf{U}^{n+1} = \mathbf{V} + \left( 1 - \sum_i \delta_i^2 \frac{\Delta V}{h^3} \right) (\tilde{\mathbf{U}} - \mathbf{V})$$

For a 3D cubic mesh  $\sum_i \delta_i^2 = \frac{1}{8}$ , so **no-slip** is obtained for  $\Delta V = 8h^3$  This determines the **No-slip radius**:

$$\mathbf{R}_{noslip} = (6/\pi)^{1/3} h \simeq 1.241h$$



## Direct forcing: fluid-particle force

Fluid momentum eq:

$$\mathbf{g}_i^{n+1} = \tilde{\mathbf{g}}^{n+1} + \rho_i^{n+1} \mathbf{a}_i \Delta t$$

$$\rho_i^{n+1} = \tilde{\rho}^{n+1}$$

Particle eqn:

$$m_p^* \frac{dV}{dt} = -\mathbf{F} + \mathbf{F}_{\text{extra}}$$

with  $m_p^* \equiv m_p - m_f$  particle mass excess (wrt. fluid.) RHS depends on  $V$  but can be solved directly,

$$\mathbf{V}^{n+1} = \mathbf{V}^n + \frac{m_f}{m_p^* + m_f} \left( \tilde{\mathbf{U}}^{n+1} - \mathbf{V}^n \right) + \frac{\mathbf{F}_{\text{extra}}}{m_p^* + m_f}$$

with  $m_f = \Delta V \sum_i \rho_i \delta_i$

## Direct forcing: a fast CUDA algorithm

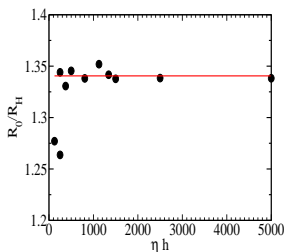
- 1 Update fluid (without particles):  $\tilde{\mathbf{U}}^{n+1}$  and  $\tilde{\rho}^{n+1} = \rho^{n+1}$ .
- 2 Update particle position,  $\mathbf{R}^{n+1} = \mathbf{R}^n + \mathbf{V}^n \Delta t$
- 3 Interpolate fluid velocity at  $\mathbf{R}$ :  $\tilde{\mathbf{U}}^{n+1} = \sum_i \delta_i \tilde{\mathbf{u}}_i^{n+1}$
- 4 Update particle velocity:  $\mathbf{V}^{n+1}$
- 5 Evaluate relative accelerations:  $\alpha$ , and node interpolations  $\mathbf{a}_i = \alpha \delta_i \Delta V / h^3$ .
- 6 Update fluid with particle force contributions:  $\mathbf{u} = \tilde{\mathbf{u}} + \mathbf{a} \Delta t$
- 7 **Straightforward generalization to  $N$  particles**

## Direct forcing: Hydrodynamic Radius from Stokes drag

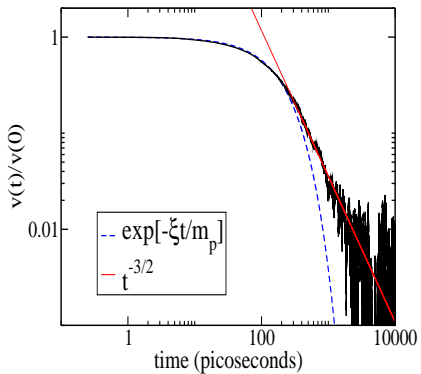
The hydrodynamic radius  $R_H$  is defined via the Stokes drag force relation

$$F = 6\pi\eta R_H V_p$$

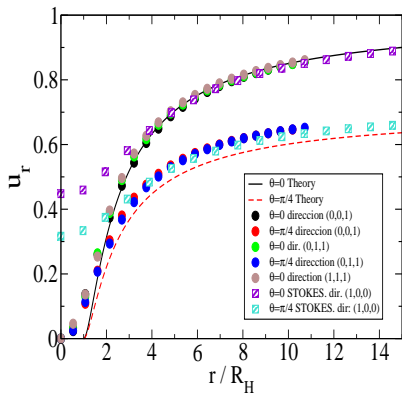
in simulations where  $V_p$  is constant and the fluid is at rest  $U_\infty = 0$ .  
We find  $R_H = R_{ns}/1.34$



## Direct forcing: Velocity decay and long-time tail

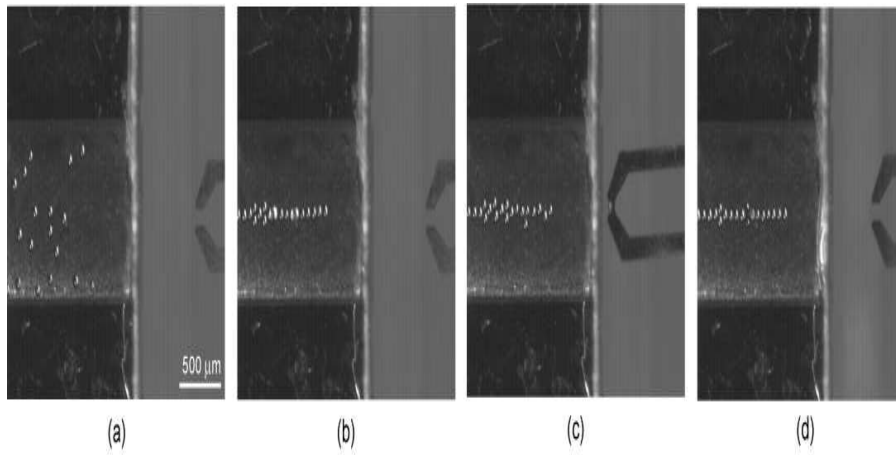


## Direct forcing: Flow lines



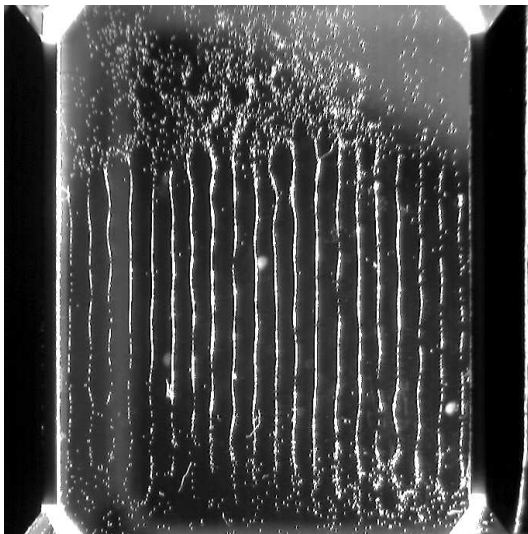
## Direct forcing: sound-particle interaction

Micromanipulation of Small Particles with Ultrasound. Jürg Dual group, ETH



## Direct forcing: sound-particle interaction

Micromanipulation of Small Particles with Ultrasound. Jürg Dual group, ETH





## Direct forcing: sound-particle interaction

Acoustic boundary layer  $\delta = \sqrt{(\nu/\omega)}$ , with  $\nu = \eta/\rho$

Wave number:  $\lambda = c 2\pi/\omega$

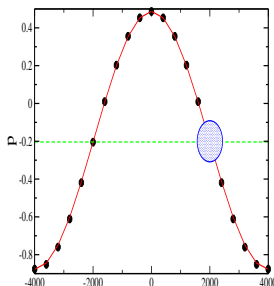
Particle radius:  $R_{NS}$

### Simulation

$R_{NS}/\lambda \simeq 0.06$ .

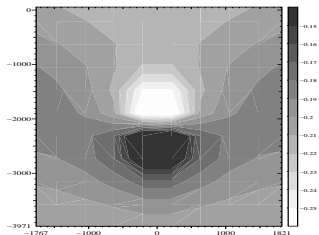
Viscous effects:  $\delta/R_{NS} \simeq 0.2$

(Stokes limit  $\delta/R_H \gg 1$  is **not** valid)

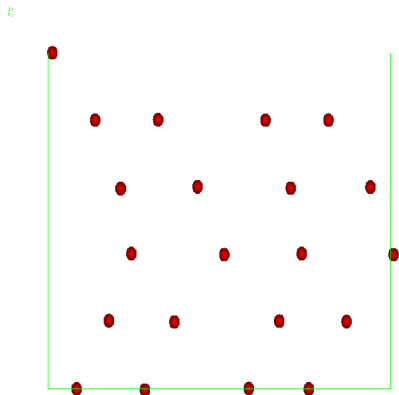


# Direct forcing: pressure perturbation around particle

Mon Oct 18 23:42:08 2010



## Direct forcing: sound-particle interaction

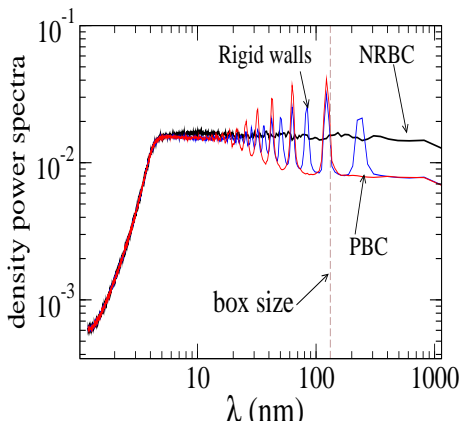


## Open Fluctuating hydrodynamics

RDB & Dejoan, Phys. Rev. E **78**, 046708 (2008)

Power spectra of density fluctuations: liquid argon @ equilibrium

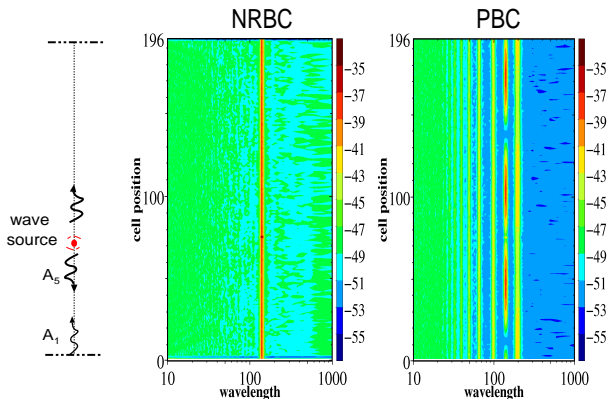
NRBC=Non-Reflecting boundary conditions



# Open Fluctuating hydrodynamics

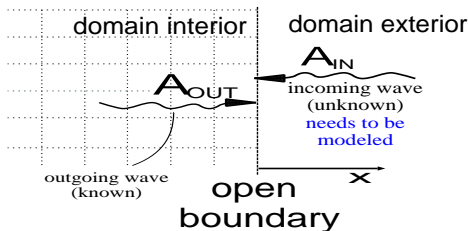
## Evacuation of sound waves using non-reflecting boundaries

RDB & Dejoan, Phys. Rev. E **78**, 046708 (2008)



## Open Fluctuating hydrodynamics

Non-reflecting boundary conditions in terms of sound modes.



- Amplitude of **sound waves**

$$A_{IN} = \frac{1}{2} \left( \frac{\delta p}{\rho_e c} - \delta u \right) \text{ moving } \leftarrow$$

$$A_{OUT} = \frac{1}{2} \left( \frac{\delta p}{\rho_e c} + \delta u \right) \text{ moving } \rightarrow$$

with  $\delta p = p - p_e$ ,  $\delta u = u - u_e$ , pressure and velocity fluctuations.

## Open Fluctuating hydrodynamics

### Non-reflecting boundary conditions for sound modes

- **Linear Navier-Stokes Eqs.**, normal-to-boundary direction,

$$\frac{\partial A_i}{\partial t} = (u \pm c) \frac{\partial A_i}{\partial x} \pm \frac{1}{\rho_e} \frac{\partial P_{xx}}{\partial x}$$

with  $i = IN \rightarrow +$  and  $i = OUT \rightarrow -$

- Amplitude variations:

$$\frac{L_i}{\rho_e c} = (u \mp c) \frac{\partial A_i}{\partial x}$$

## Open Fluctuating hydrodynamics

$$\frac{\partial A_i}{\partial t} + \frac{L_i}{\rho_e c} = \pm \frac{1}{\rho_e} \frac{\partial P_{xx}}{\partial x}$$

Amplitude variations,

$$L_{OUT} = (u - c) \frac{\partial A_{OUT}}{\partial x} \text{ Measured within domain}$$

$$L_{IN} = K(\rho c A_{IN}) \text{ Modelled}$$

$$K = \frac{\nu_L}{(0.4\Delta x)^2} \text{ Satisfies FD balance}$$



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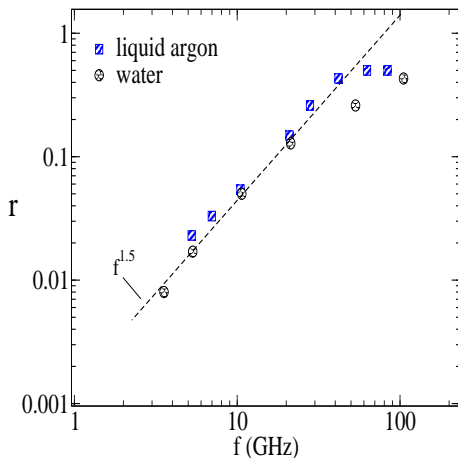
**NRBC Eqs. for boundary cells,**

$$\text{density} : \frac{\partial \rho}{\partial x} = 0$$

$$\text{velocity} : \frac{\partial u}{\partial t} + \frac{1}{2\rho_e c} (L_{OUT} - L_{IN}) = 0$$

## Open Fluctuating hydrodynamics

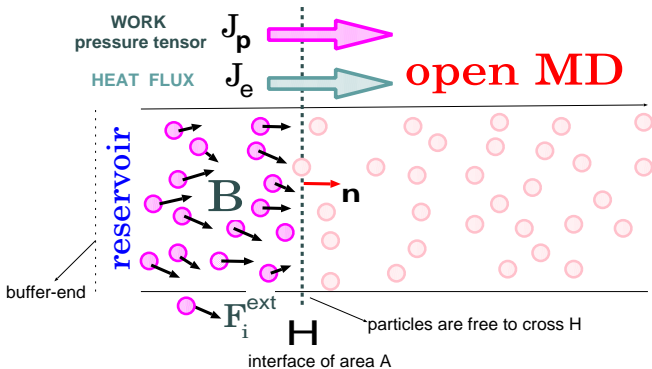
NRBC Reflection coefficient.



# Open MD

## via external forces

$$m\ddot{\mathbf{r}}_i = \mathbf{f}_i(\{\mathbf{r}\}) + \mathbf{f}_i^{\text{ext}}$$



## State-Coupling

(see: Thomsom and O'Connel and Mark Robbins' group)

### Scope

- **CFD Research:** effects of molecular domain onto the mean flow.
- **Priority:** The external flow imposed into the molecular region.
- **Mass flux:** Imposed to MD using continuum expression:  
 $A\rho V_n$ .
- **NO molecular fluctuations**
- **Impose** external velocity  $\mathbf{V}$  at the buffer  $\bar{\mathbf{v}} \equiv \frac{1}{N_B} \sum_{i \in B} \mathbf{v}_i$

## State-Coupling

### Method

- Constrained dynamics:  $m\ddot{\mathbf{r}}_i = (\mathbf{f}_i - \bar{\mathbf{f}}) - \xi(\mathbf{v}_i - \mathbf{V})$
- External force:  $\mathbf{f}_i^{\text{ext}} = -\bar{\mathbf{f}} - \xi(\mathbf{v}_i - \mathbf{V})$
- Mean buffer velocity:

$$\frac{d\bar{\mathbf{v}}}{dt} = -\gamma(\bar{\mathbf{v}} - \mathbf{V})$$

$\bar{\mathbf{v}}$  converges to  $\mathbf{V}$  exponentially (at rate  $\gamma = \xi/M_B$ ); and instantaneously if  $\gamma = 1/\Delta t$

## Thermodynamics of State-Coupling

Input power

$$\dot{E} = \sum_{i \in B} \mathbf{f}_i^{\text{ext}} \cdot \mathbf{v}_i$$

External force

$$\mathbf{f}_i^{\text{ext}} = -\bar{\mathbf{f}} - \xi (\mathbf{v}_i - \mathbf{V})$$

where

$$\bar{\mathbf{f}} = \frac{1}{N} \sum_{i \in B} \mathbf{f}_i = M \frac{d\bar{\mathbf{v}}}{dt}$$

## Thermodynamics of State-Coupling

Assume  $\bar{\mathbf{v}} \simeq \mathbf{V}$

$$\dot{E} = -N\bar{\mathbf{f}} \cdot \bar{\mathbf{v}} - \xi \sum_{i \in B} (\mathbf{v}_i - \bar{\mathbf{v}})^2$$

Use equipartition  $3kT = \langle (\mathbf{v}_i - \bar{\mathbf{v}})^2 \rangle$  and  $\langle \bar{\mathbf{f}} \bar{\mathbf{v}} \rangle = M \langle \frac{d\bar{\mathbf{v}}}{dt} \bar{\mathbf{v}} \rangle = 0$  to get:

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$$\frac{d\langle E \rangle}{dt} = -3 \frac{\xi}{m} NkT$$

Exponential freezing (very fast,  $\xi/m \gg \xi/M = \gamma$ ).

**Thermostatting is required** (DPD better than simple velocity rescaling!)



## Flux-Coupling

(See: Flekkoy, RD-B and Coveney, Phys. Rev. E, 72, 026703 (2005))

### Scope

- **Molecular research:** effects of flow on molecular domain.
- **Priority:** avoid external artifacts into molecular domain
- **Mass flux:** Measured from MD; naturally arises from pressure gradient across the interface
- **Molecular fluctuations** (mass, momentum, energy)
- **Imposes:** Flux across interface of area  $A$  and (inwards) surface vector  $\mathbf{n}$
- **Momentum** flux (force/area)  $\mathbf{P}_n = \mathbf{P} \cdot \mathbf{n}$
- **Heat** flux (energy/time)  $\dot{Q}_e = \mathbf{q} \cdot \mathbf{n}$

## Flux-Coupling

(PRE, 72, 026703 (2005) **Method**

- External force to buffer particles:  $\mathbf{f}_i^{\text{ext}} = \bar{\mathbf{f}}_{\text{ext}} + \tilde{\mathbf{f}}_{\text{ext}}$
- Momentum transfer by the average external force

$$\bar{\mathbf{f}}_{\text{ext}} = \mathbf{P}_n A / N_B$$

- Heat transfer by the fluctuating external force

$$\tilde{\mathbf{f}}_{\text{ext}} = \frac{\mathbf{v}_i}{\sum_{i \in B} v_i^2} \dot{Q}_e$$

- Momentum and energy due to particle insertion/deletions can be taken into account (**exact balance**).

## Thermodynamics of Flux-Coupling

Energy input over  $\Delta t$

$$\Delta E = \sum_{i \in B} \mathbf{f}_i^{\text{ext}} \cdot \mathbf{v}_i \Delta t + \sum_k e_k$$

$$\mathbf{f}_i^{\text{ext}} = A \mathbf{P}_n / N + \frac{\mathbf{v}_i}{\sum_{i \in B} v_i^2} \dot{Q}_e$$

$$\Delta E = A \mathbf{P}_n \cdot \bar{\mathbf{v}} \Delta t + \dot{Q}_e \Delta t + \sum_k e_k$$

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Entropy change (quasi-stationary,  $\dot{Q}_e$  not so large)

$$T\Delta S' = \sum_k e_k - \mu\Delta N \text{ Particle insertions}$$

$$T\Delta S = \dot{Q}_e \Delta t + T\Delta S' \text{ Total}$$

## Thermodynamics of Flux-Coupling

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## Thermodynamics of Flux-Coupling

Energy input

$$\Delta E = A\mathbf{P}_n \cdot \bar{\mathbf{v}}\Delta t + T\Delta S + \mu\Delta N$$

Pressure and stress (tangential external force)

$$\begin{aligned}\mathbf{P}_n &= p\mathbf{n} + P_t\mathbf{t} \\ A\mathbf{P}_n \cdot \bar{\mathbf{v}}\Delta t &= p(A\bar{\mathbf{v}} \cdot \mathbf{n}\Delta t) + AP_t\bar{\mathbf{v}} \cdot \mathbf{t}\Delta t\end{aligned}$$

Hence,

$$\Delta E = -p\Delta V + T\Delta S + \mu\Delta N + \text{Heat dissipated by shear}$$

Flux coupling is consistent with equilibrium thermodynamics for open systems.

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- The amount of HEAT and WORK done into the MD system is exactly controlled

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Isobaric ensemble  $\mathbf{P}_n = p\mathbf{n}$

Outlet B.C., Hybrids

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Dynamics of confined systems

Isobaric ensemble  $\mathbf{P}_n = p\mathbf{n}$

Outlet B.C., Hybrids

Constant enthalpy  $\dot{Q}_e = 0$   
 $(\Delta N = 0)$

Joule-Thompson, MD-calorimeter

$$\Delta H = \Delta E + p\Delta V = 0$$

## Flux-coupling: OPEN MD in generalized ensembles

- The amount of HEAT and WORK done into the MD system is exactly controlled
- The system communicates with the exterior at its boundaries, like a real system.

Grand canonical  $\mu_B VT$

Dynamics of confined systems

Isobaric ensemble  $\mathbf{P}_n = p\mathbf{n}$

Outlet B.C., Hybrids

Constant enthalpy  $\dot{Q}_e = 0$   
( $\Delta N = 0$ )

Joule-Thompson, MD-calorimeter

$$\Delta H = \Delta E + p\Delta V = 0$$

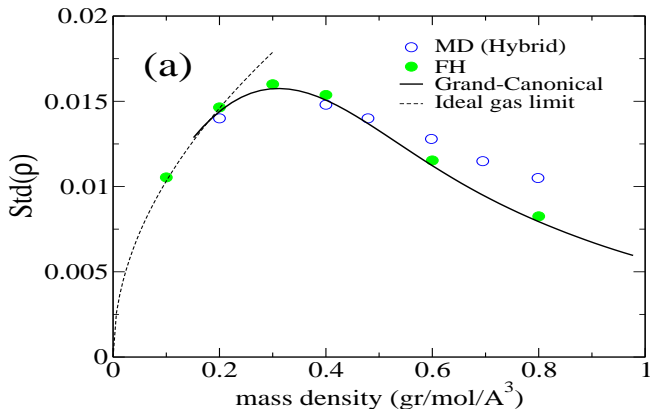
Constant heat flux:  $\dot{Q}_e$

Melting, ice formation,  
heat exchange at complex surfaces

## Density fluctuations (MD-FH hybrid)

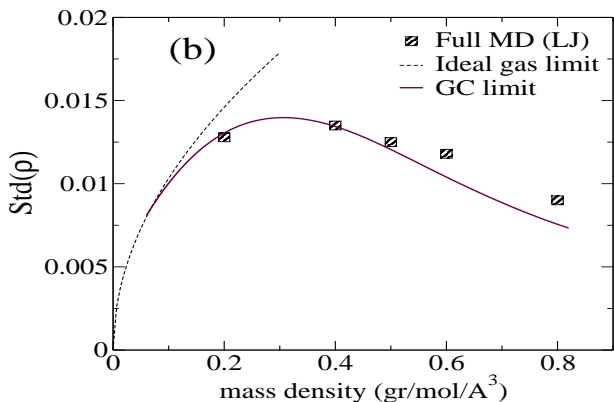
Standard deviation of argon density,  $T = 300K$

RDB and G.Fabritiis et al. PRE, **76** (2007)



## Density fluctuations (Full MD)

Standard deviation of argon density,  $T = 300K$   
Subvolume of a large PBC box



## Open MD

### Density profile at the buffer

- The external force on a molecule  $i$  in the buffer:

$$\mathbf{f}_i^{ext} = \frac{g(x_i)}{\sum_{i \in B} g(x_i)} \mathbf{F}^{ext} \quad (\text{with } \mathbf{F}^{ext} = A\mathbf{P} \cdot \mathbf{n})$$



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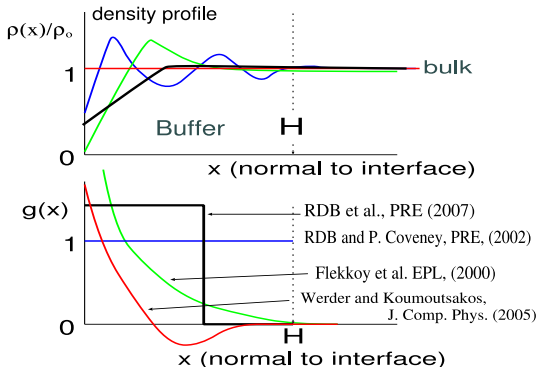
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- The buffer density profile is controlled by the force distribution  $g(x)$ .
- Any  $g(x) \neq \text{cte}$  introduces **spurious heat** into the system and requires thermostats.

## Open MD

## Density profile at the buffer

$$\mathbf{f}_i^{ext} = \frac{g(x_i)}{\sum_{i \in B} g(x_i)} \mathbf{F}^{ext} \quad (\text{with } \mathbf{F}^{ext} = A\mathbf{P} \cdot \mathbf{n})$$



## Open MD

### Mass control at the buffer

The average buffer mass is controlled to a fixed value  $\langle M_B \rangle$

$$\frac{\Delta M_B}{\Delta t} = \frac{1}{\tau_B} (\langle M_B \rangle - M_B)$$

with  $\tau_B \simeq [10 - 100]fs$  (faster than any hydrodynamic time).

- Deletion:  $\Delta M_B < 0$  (also particles crossing the buffer-end)
- Insertion:  $\Delta M_B > 0$ 
  - Small solvent molecules: **USHER algorithm** for
  - Large molecules (star polymers): **Adaptive Resolution**

## Open MD

### Mass control at the buffer

### Particle insertion by the **USHER algorithm**

J. Chem. Phys. **119**, 978 (2003) spherical molecules

J. Chem. Phys. **121**, 12139 (2004) for water

- Insert a new molecule at target potential energy  $E_T$  (usually  $E_T = e(\rho, T)$  mean energy per particle)

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- **Negligible insertion cost** < 1% total CPU (LJ), ~ 3% (water).
- **Very fast**: water into water at low energy ( $E_T = e$ ) requires 100 iterations ( $10^5$  faster than random insertion)

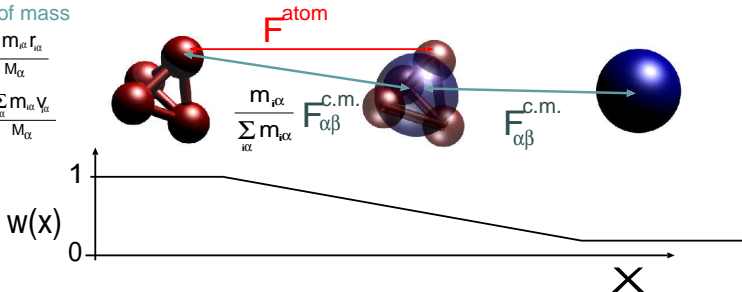
## Adaptive Resolution Scheme

Praprotnik, Delle Site, Kremer, Annu. Rev. Phys. Chem. 59, 545 (2008)

center of mass

$$R_{\alpha} = \frac{\sum_{i\alpha} m_{i\alpha} r_{i\alpha}}{M_{\alpha}}$$

$$V_{\alpha} = \frac{\sum_{i\alpha} m_{i\alpha} v_{i\alpha}}{M_{\alpha}}$$

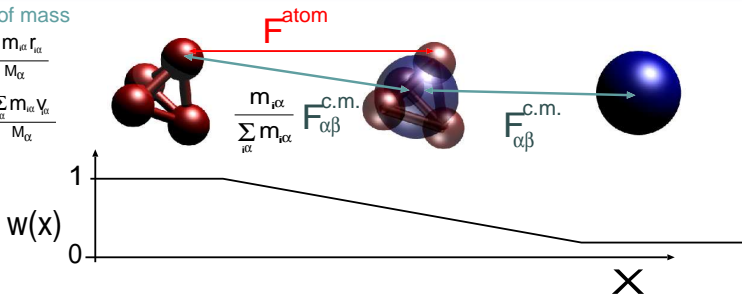


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$$\mathbf{V}_\alpha = \frac{\sum_{i\alpha} m_{i\alpha} \mathbf{v}_{i\alpha}}{M_\alpha}$$



$$\mathbf{F}_{\alpha\beta} = w(x_\alpha)w(x_\beta) \sum_{i\alpha j\beta} \mathbf{F}_{i\alpha j\beta}^{\text{atom}} + [1 - w(x_\alpha)w(x_\beta)] \mathbf{F}_{\alpha\beta}^{\text{c.m.}}$$

$$\mathbf{F}_{i\alpha j\beta}^{\text{atom}} = - \frac{\partial U^{\text{atom}}}{\partial \mathbf{r}_{i\alpha j\beta}} \quad \text{Atomistic}$$

$$\mathbf{F}_{\alpha\beta}^{\text{c.m.}} = - \frac{\partial U^{\text{c.m.}}}{\partial \mathbf{R}_{\alpha\beta}} \quad \text{Coarse - Grained}$$



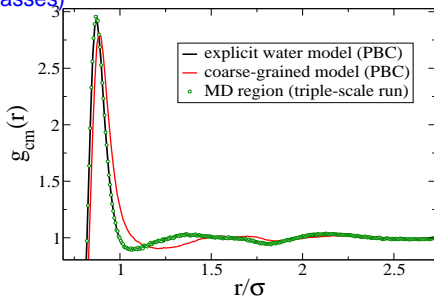
## Open MD with AdResS

### The *adaptive buffer*

does not require accurate fits for the CG and HYB models  
 RDB, Kremer, Praprotnik, J.Chem.Phys. **131**, 244107 (2009)

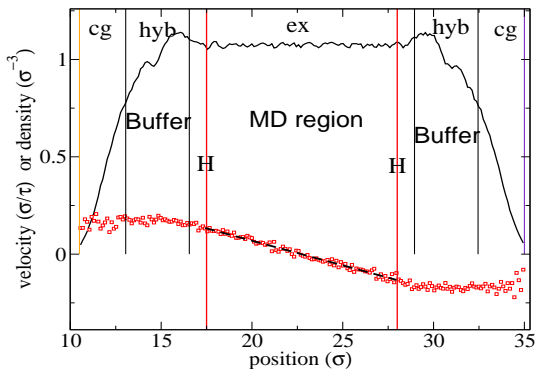
Viscosities (oxygen-LJ units) CG  $\eta=20$   
 EX  $\eta=45$  — Flexible TIP3P water model

Radial distribution functions  
 (center of masses)



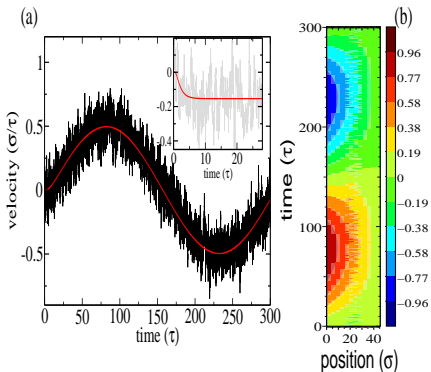
## HybridMD-AdResS triple scale

RDB, Kremer, Praprotnik, J.Chem.Phys. **131**, 244107 (2009)

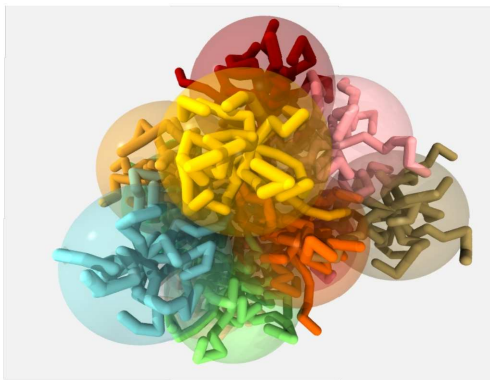


## HybridMD-AdResS triple scale

Simulation of TIP3P water under oscillatory shear RDB, Kremer, Praprotnik, J.Chem.Phys. **131**, 244107 (2009)



## Melts of star polymers via OPEN MD-AdResS

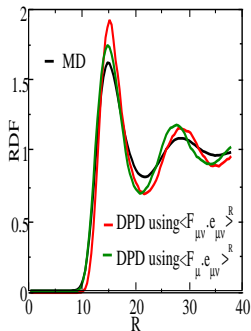
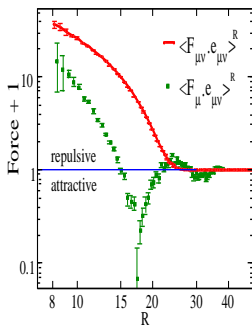




## Melts of star polymers via OPEN MD-AdResS

[R.D-B and Praprotnik, in preparation]

Star 12-6  $\phi=0.2$

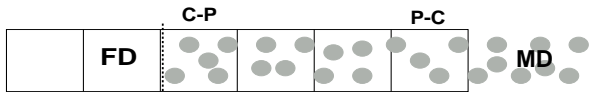


## Hybrid particle-continuum schemes: alternatives

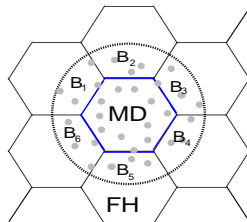
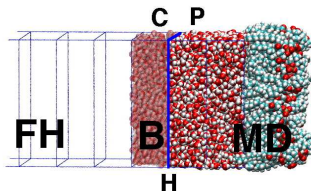
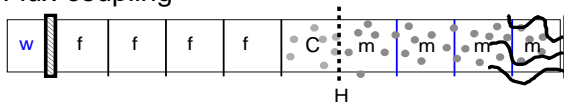
- **State scheme:** Non-conservative, no fluctuations (requires averaging), incompressible.
- **Flux scheme:** Conservative, fluctuations, compressible.

## Hybrid particle-continuum schemes: set-up

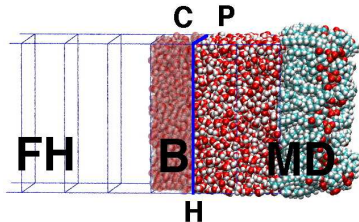
State-coupling



Flux-coupling



## Continuity in flux schemes



The continuum solver, schematically

$$\Delta\Phi_i = \Delta t NS [\{\Phi_j\}] + \delta_{fC} \Delta\phi^{MD}$$

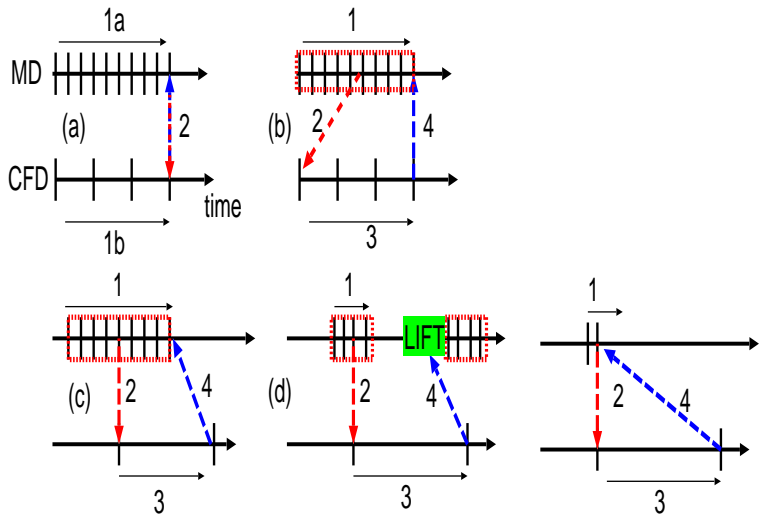
Relaxation of particle transfers towards C

$$\Delta M^{MD} = \frac{\Delta t_c}{\tau_M} (\Delta M_H^{MD} - \Delta M_H^{NS})$$

$$\text{where } \Delta M_H^{NS} = -A\rho_H \mathbf{V}_H \cdot \mathbf{n} \Delta t$$

$$\Delta \mathbf{V}^{MD} = \frac{\Delta t_c}{\tau_v} (\langle \mathbf{v}_C^{MD} \rangle_{[\delta t, \tau]} - \langle \mathbf{V}_C \rangle_{[\Delta t, \tau]})$$

## Hybrid particle-continuum schemes: Time coupling



## Hybrid MD-Fluctuating Hydrodynamics

### Matching stress fluctuations via Green-Kubo relations

- **Molecular dynamics:** decorrelation time  $\tau_c \sim 100\text{fs}$  (simple liquids)

$$\langle J_{MD}^2 \rangle = \frac{\eta k_B T}{V \tau_c} \text{ with, } \tau_c \equiv \frac{\int_0^\infty \langle J(t) J(0) \rangle dt}{\langle J(0)^2 \rangle}$$

- **Fluctuating hydrodynamics:** decorrelation time  $\Delta t_{FH}/2$ ,

$$\langle J_{FH}^2 \rangle = \frac{2\eta k_B T}{V \Delta t_{FH}}$$

Balance stress fluctuations,  $\langle J_{MD}^2 \rangle = \langle J_{FH}^2 \rangle$ :

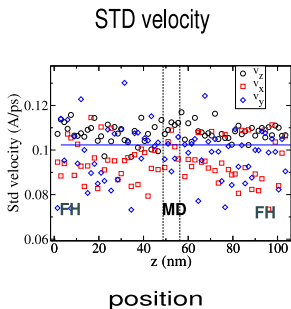
$\Delta t_{FH} = 2\tau_c = \delta t_S$  Sampling time = twice MD decorrelation time

In general,  $\Delta t_c = n_{FH} \Delta t_{FH} = N_s \delta t_s$

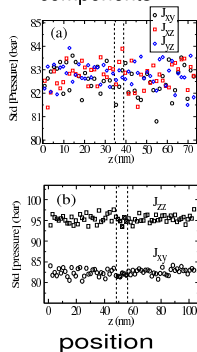
## Hybrid MD-Fluctuating Hydrodynamics: equilibrium state

Standard deviation of velocity (kinetic temperature)  
liquid argon @  $T = 300K$

RDB and G.Fabritiis et al. PRE, **76** (2007)



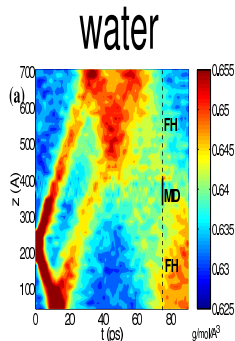
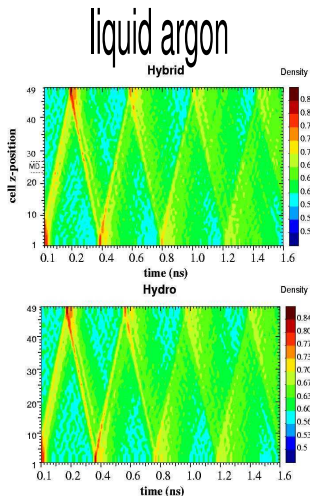
STD Stress tensor components



# Hybrid MD-Fluctuating Hydrodynamics

## Some test cases: sound

De Fabritiis, R.D-B and P. Coveney, PRL, 97 (2006)

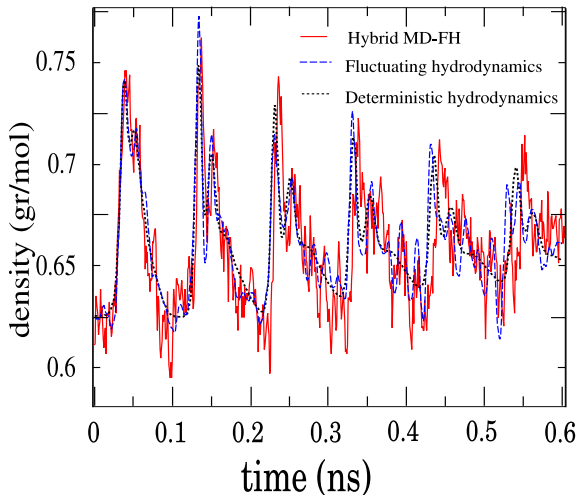




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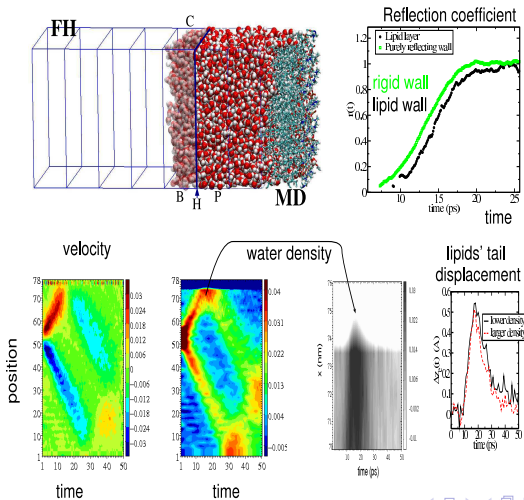


# Hybrid MD-Fluctuating Hydrodynamics

## Collision of sound waves against DMPC lipid layer

De Fabritiis, R.D-B and P. Coveney, PRL, 97 (2006)

RDB et al, Proc IMechE, Part C: J Mech. Eng. Sci. **222** (2008)



## Conclusions

- New tools are required to study the effects of sound in soft matter.
- Molecular information about effective friction, draining and slip boundary conditions is required to feed micron-scale simulations.
- Sound simulations require **open systems**: OPEN MD, OPEN FH possibly used in combination with ADDRESS
- Sound at micron and submicron scales: DIRECT FORCING in compressible flow.
- Sound at nano-scale: HYBRID MD